Thermal compensation of the optical RF delay line for the SPS transverse damper

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Motivation

- SPS reference RF signals are generated in BA3
- SPS damper installed in BA2 (opposite direction than the beam is circulating)
 RF signals
- lons use a sophisticated RF modulation scheme to accelerate "fixed frequency acceleration"
- Reference RF signals and the beam pickup signals have to arrive to the electronics at the same time





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Motivation

 RF signals and the beam are synchronous in BA3

• They have to be made synchronous also in BA2









Fibre RF delay line

 $\circ~$ Delays of several tens of μs can be easily obtained using analogue optical transceivers and single mode optical fibres



14.8 μs fibre coil (3 km) with analogue Spinner optical transceiver



Purpose of fibre thermal compensation

- Fibre thermal drift is too large for our application, temperature effects have to be compensated
- $_{\odot}~$ Group delay of 3 km long (~14.8 $\mu s)$ optical fibre was measured in a thermal chamber



 Normalized polynomial fit: τ_{dNORM} = -3.265197x10⁻⁸ t² + 1.015301x10⁻⁵ t + 9.997133x10⁻¹ [1; °C]



Requirements for temperature stability

- To meet the desired stability of group delay, temperature control must be very tight.
- Tolerated delay drift for correct damper operation is typically ±125 ps.





Maximum fibre temperature variation as a function of total fibre delay and tolerated delay drift.



Design of thermally insulated enclosure

- For practical reasons the fibre temperature is stabilized above the ambient
- Thermally insulated enclosure, housing 4 fibre coils have been designed
- To increase the thermal mass (and inertia), the enclosure is made of aluminium bars





Design of thermally insulated enclosure

- Heating is provided by power MOSFETs mounted to the aluminium bars
- Each fibre slot has a heater board mounted on both sides
- Total 8 heater elements



Each heater boards is equipped by a PT1000 temperature probe



Temperature controller

- Design goal was to reach a temperature stability better than ±0.25 °C
- Controller is build as a fully analogue circuit
- Precision parts are used, such as PT1000, instrumentation amplifiers, voltage reference...
- To meet this requirements PI topology was used
- The topology was carefully designed such that temperature drifts in various parts of the circuit are cancelling-out





Controller test circuit

• For testing the performance of design controller prototype was build





- Step response (switch on transient)
- Constant ambient temperature of 22 °C
- Setpoint temperature of 45 °C





Stability at constant ambient temperature 22 °C





- Response to a large external perturbation
- Setpoint temperature 45 °C
- Variation of ambient temperature from 15 to 29 °C when the thermal chamber was heating up





- Response to a large external perturbation
- Setpoint temperature of 45 °C
- Variation of ambient temperature from 31 to 17 °C when the thermal chamber was cooling down





Captured analogue regulator signals during initial heat up from 23 to 45 °C





Project status

- Controller prototype successfully tested
- Final PCB designed and production file ready to sent out
- Mechanical design drawings being finalized by P. Hofer
- Whole unit ready to be sent for production and installation in BA2



Project status





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High voltage divider signal conditioner

- Second project I was working on during my stay
- Conditioning of RF-divider signals of the SPS transverse damper tetrode amplifier. Analogue and RF circuitry, 20 MHz bandwidth, fan-out, multiple 50 Ω line drivers.
- Prototype assembled, ready for tests













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